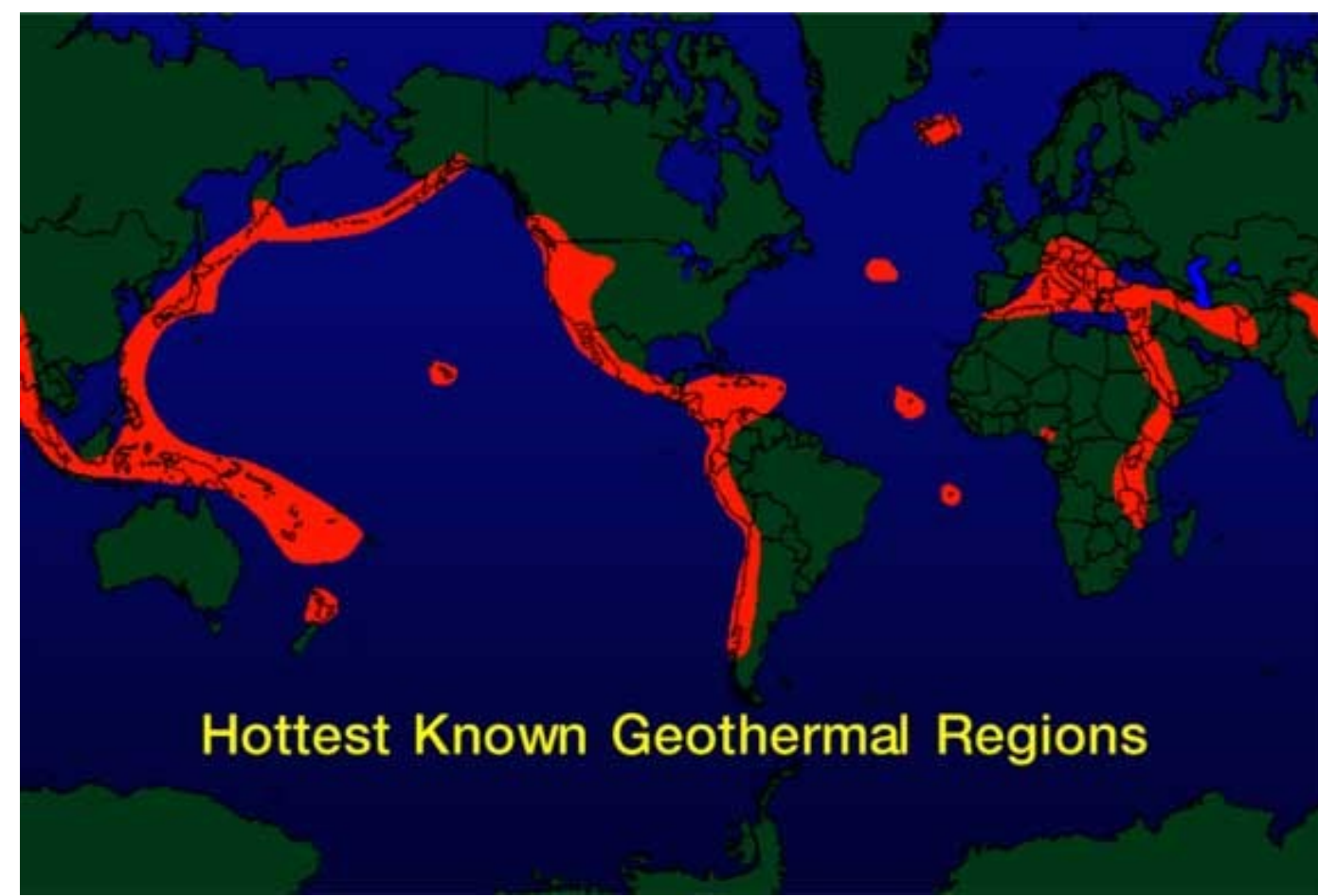
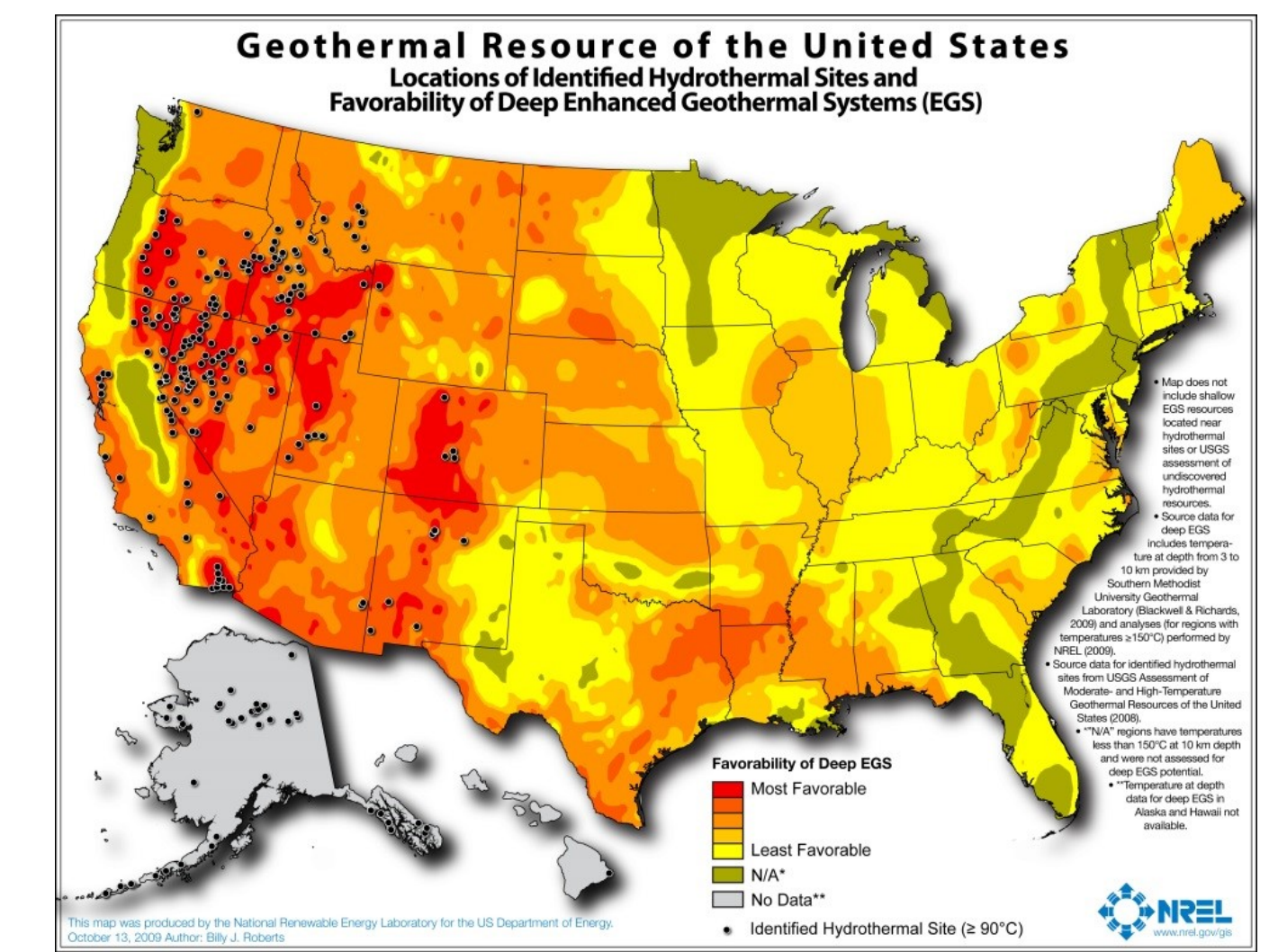


Heat Transfer Model Estimating Energy Extraction from a Closed-Loop Geothermal System*

Lea-Der Chen, Ph.D.
Texas A&M University – Corpus Christi
Corpus Christi, TX 78412-5806



A heat transfer model is established for calculation of closed-loop geothermal systems. Of which the heat exchange sections have very large length-to-diameter (L/d) ratios. The model is used to estimate heat extraction from the system described in U.S. Patent 8,991,488. For quasi-steady-state heat transfer analysis, it shows that the soil-side thermal resistance is much larger than the liquid-side thermal resistance of the closed-loop system described in U.S. Patent 8,991,488. Conversely, the rate of energy extraction is limited by the soil-side heat transfer. For soil-side heat transfer, a simplified heat transfer model is established. The model is based on Kelvin's line-source model to account for large L/d ratios of the system, which exceeds 10,000, and to account for time-dependency of the energy extraction. The results show that for a pre-set outer-wall temperature of the heat exchange section, the total amount of energy extraction depends on the energy extraction rate. Higher energy extraction rates result in shorter periods of operation. For a fixed rate of energy extraction, higher surrounding temperatures result in longer periods of operation. The model also identifies a non-dimensional parameter that can be used as a scaling parameter for different diameters of the heat exchange section.



* This work was supported, in part, by InnerGeo, LLC.

Specific Objectives

- Develop mathematical model to estimate heat extraction from closed-loop geothermal systems that are characterized by
 - Large aspect ratios, i.e., large length-to-diameter ratios, presenting challenges to numerical calculation
 - Time scale of years
 - Complex physical properties

Case Study – InnerGeo, U.S. Patent 8,991,488 B2

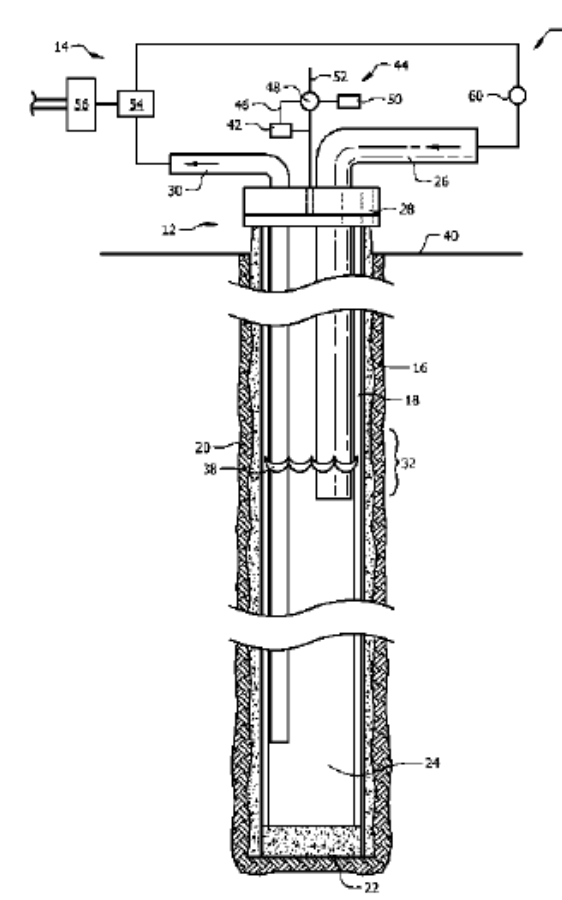


Table 1. Summary of Geometric and Operating Parameters

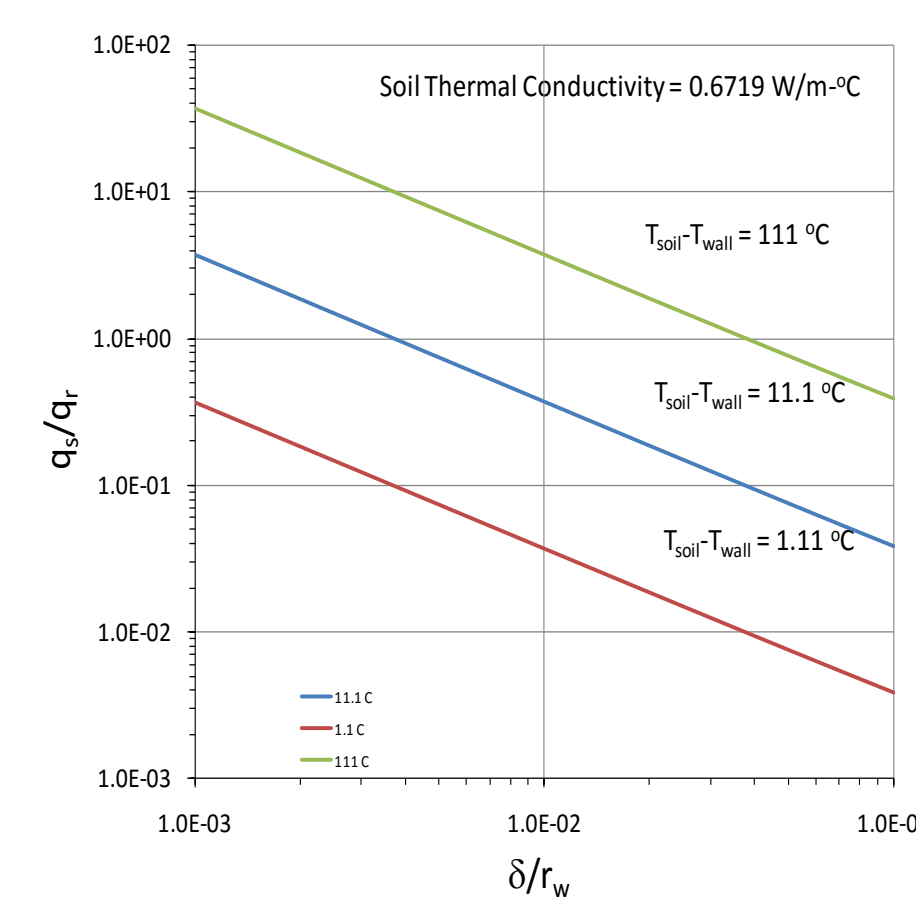
Geometry	
Well diameter:	17 in
Injection tube:	8 in
Production (heated water) tube:	3 in
Heated tube section (horizontal):	5280 ft
Operating condition	
Feed water:	200 F
Production water:	350 F
Flowrate:	1000 gallon/min

Quasi-Steady State Water-Side Heat Transfer

- Water-side heat transfer
 - Heat-load and overall heat transfer coefficient needed
 - $q_r = \rho Q (h_e - h_i) = 20.4 \text{ MW}_{th}$
 - $U_r = q_r / (A \Delta T_{lm}) = 201.3 \text{ W/m}^2\text{C}$
 - Tube heat transfer coefficient – water properties
 - $Nu = 0.023 Re^{0.8} Pr^{0.4}$
 - $U_r = 2,117 \text{ W/m}^2\text{C} \gg 201.3 \text{ W/m}^2\text{C}$
- Water-side can deliver heat transfer needed

Quasi-Steady State Soil-Side Heat Transfer

- Soil-side
 - Heat transfer from soil to wall
 - $q_s = 2\pi L k_s (T_s - T_w) / \ln(r_p / r_w)$
 - Thermal penetration length
 - $\delta = r_p - r_w$
 - Results showing that heat load can be met if
 - $T_s - T_w = 11.1$ or $111 \text{ }^\circ\text{C}$ and $\delta / r_w < 0.4$ or 0.04 , respectively
 - $T_s - T_w = 1.11$ and $\delta / r_w < 0.001$



Line Source Analysis – Modified Kelvin's Theory

$$T_s - T_w = q / (4\pi k) E_1(r^2 / (4\alpha_{grd} t)); E_1(r^2 / (4\alpha_{grd} t)) = \ln(4\alpha t / r^2) - 0.5772$$

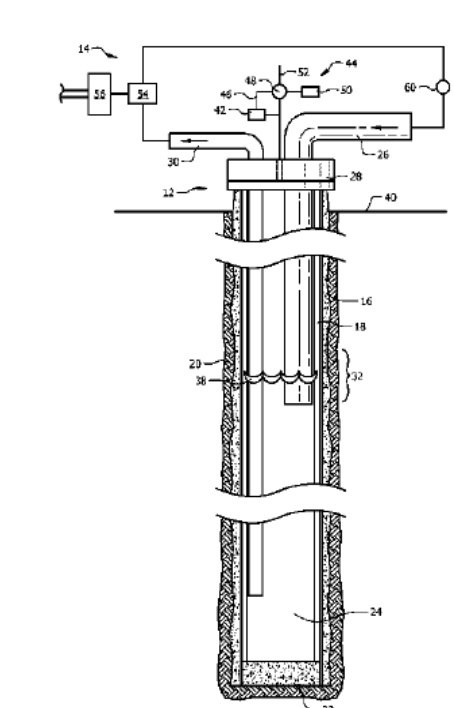
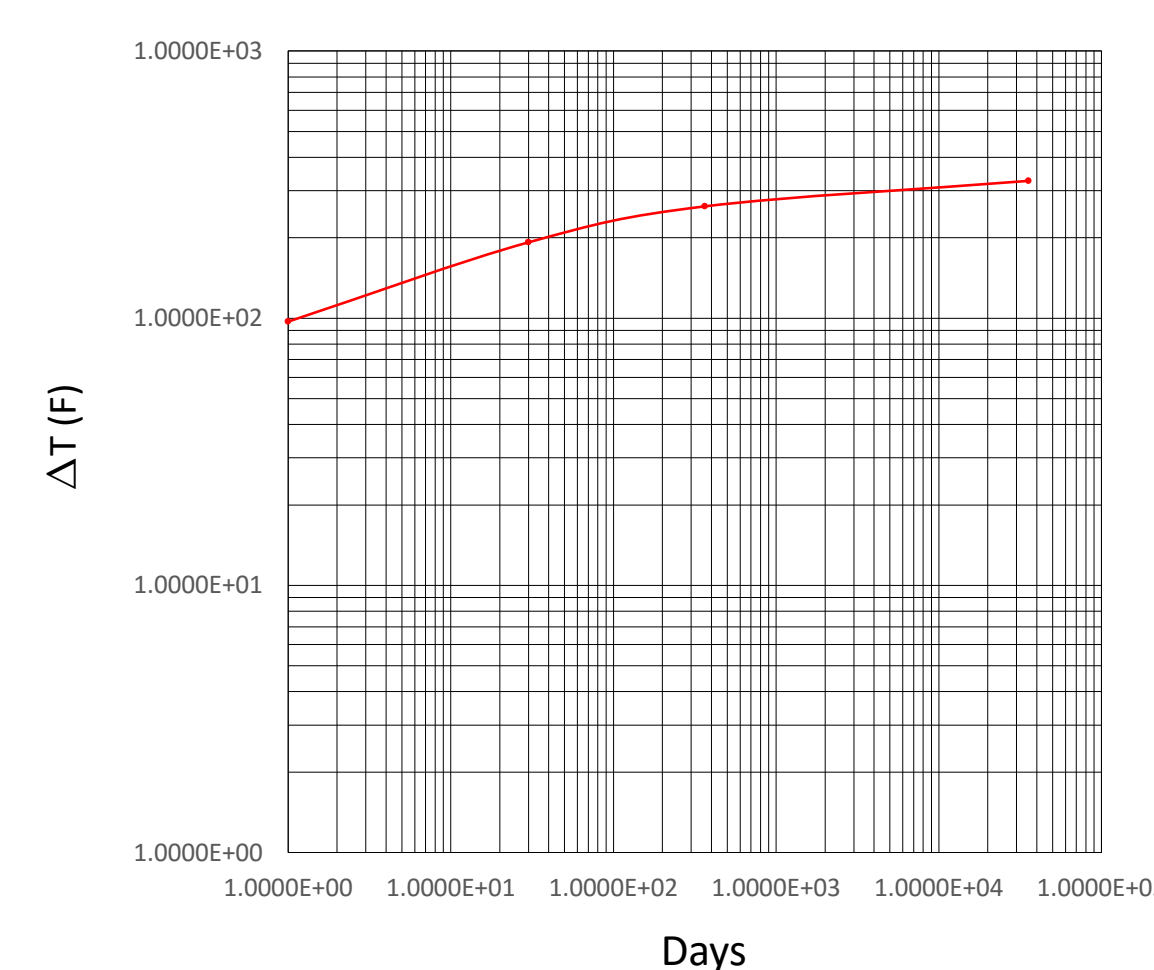


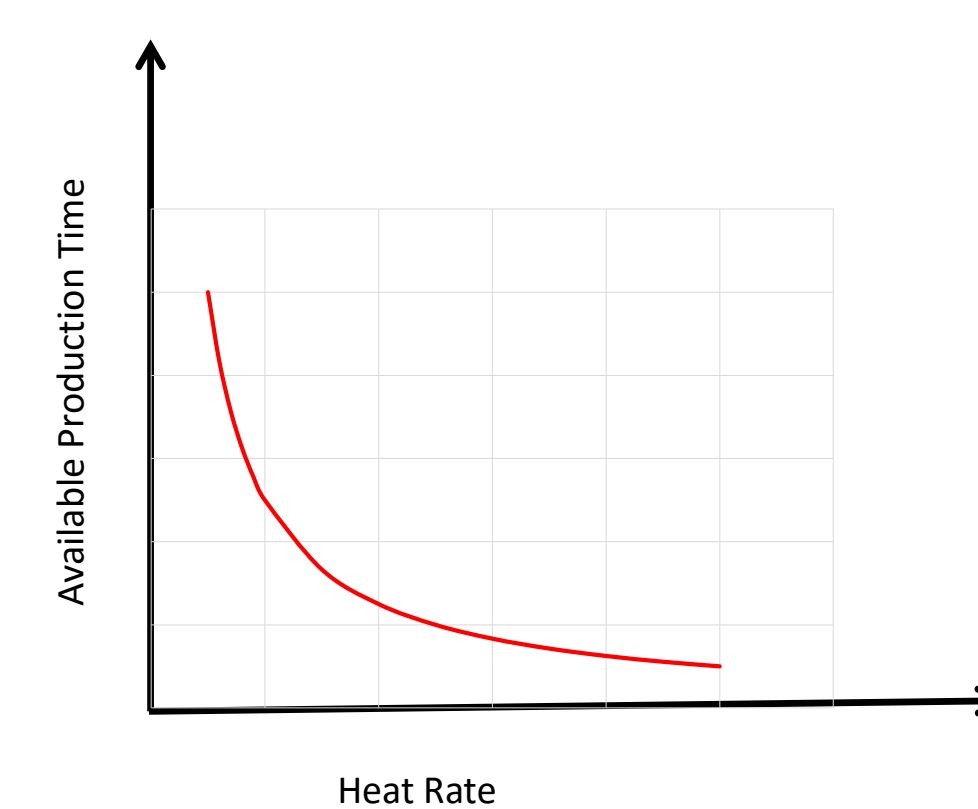
Table 2. Geometric and Operating Parameters – 408 kW_{th}

Geometry	
Well diameter:	7 in
Injection tube:	3 in
Production (heated water) tube:	2 in
Heated tube section (horizontal):	5280 ft
Operating condition	
Feed water:	200 F
Production water:	350 F
Flowrate:	20 gallon/min

Soil Temperature Requirements



Heat Rate vs. "Available" Production Time



- "Available" production time decreases with increasing heat rate extraction
- Heat transfer analysis can assist setting the operating condition in design stage
- Heat transfer analysis can also assist revenue estimates and ROI

Texas A&M University – Corpus Christi



L.-D. Chen
361-825-3046
LD.Chen@tamucc.edu