

Heat Recovery from Sedimentary Formations

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Motivation

- **Studies show surface area for heat transfer crucial to energy production**
 - Sediment A >> Fracture A
- **Existing infrastructure reduces cost**
 - Wells, Separators, Reinjection
- **Potential to extend “EGS” to 6-10 new states**

Summary of Cases Studied

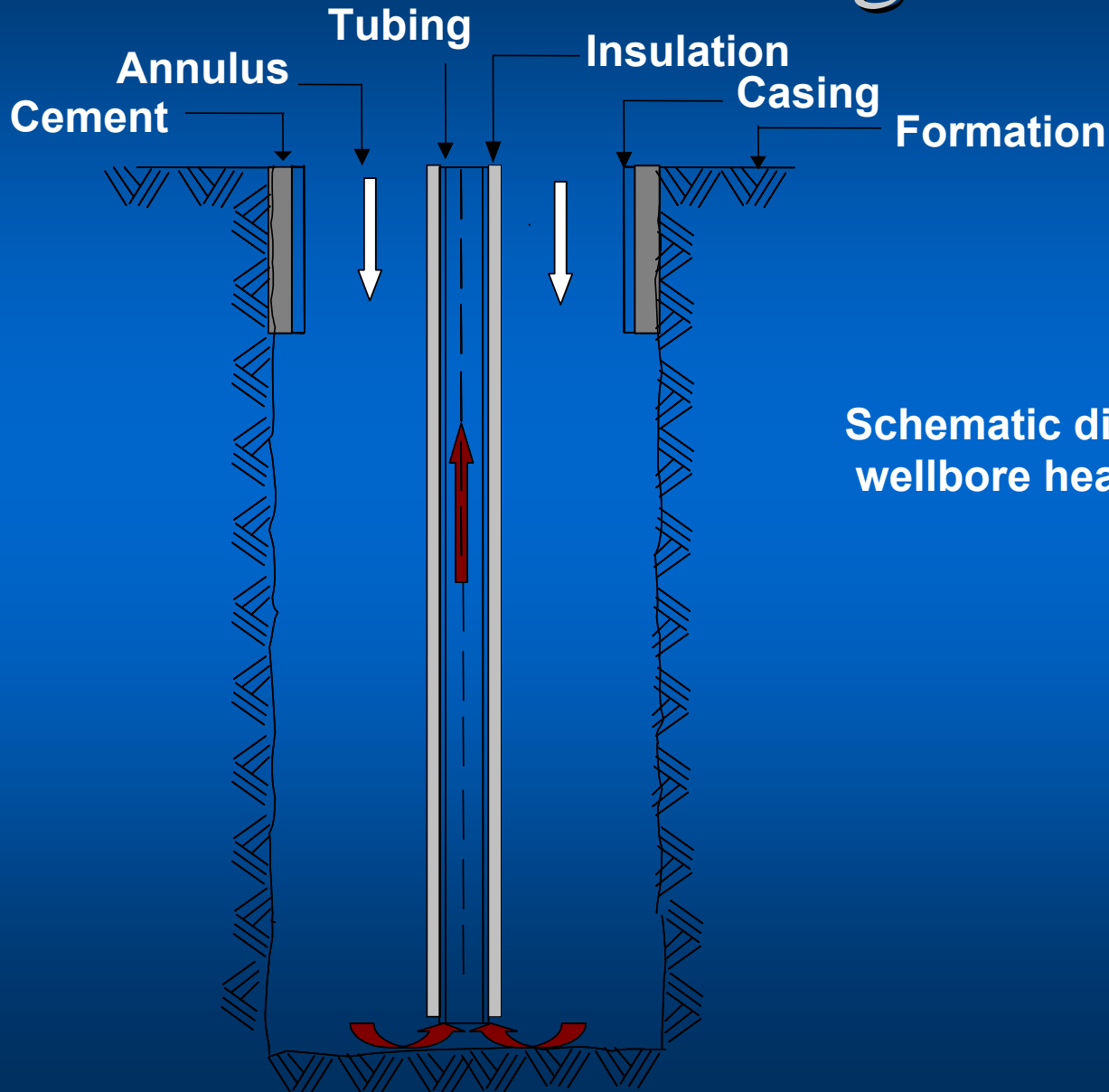
- **Single wellbore heat exchangers**
- **Advanced well technologies**
- **Single wellbore fluid extraction**
- **Injection/Production well pairs**

Parametric Sensitivity Study in Wellbore Heat Exchangers

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Wellbore Heat Exchanger Model



Schematic diagram of the wellbore heat exchanger

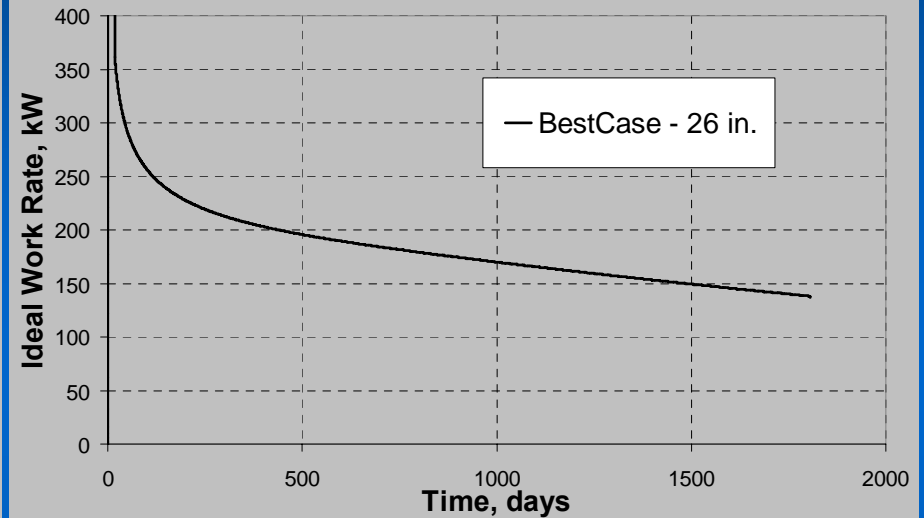
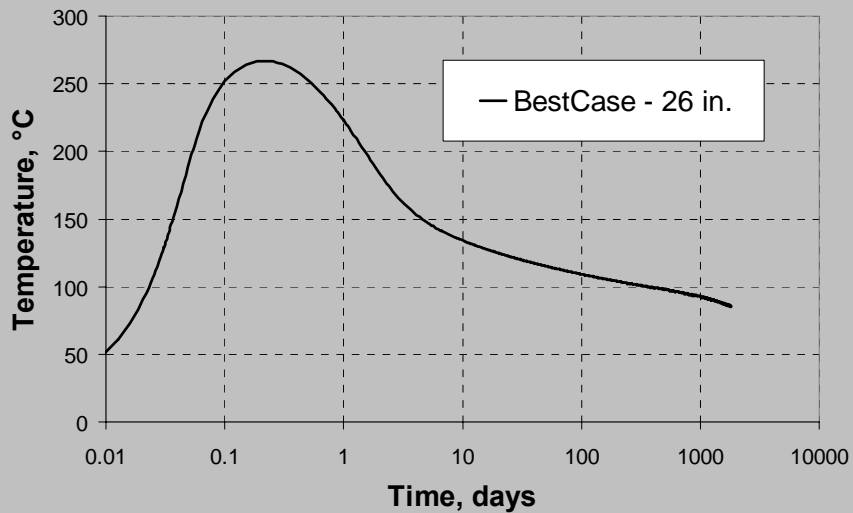
Parametric Sensitivity Study

- **Circulation Rate**
- **Wellbore diameter**
- **Tubing properties**
- **Working fluid properties**
- **Heat flux / wellbore depth**
- **Formation types**

Optimal Parameters from Studies

- **Circulation Rate** ➤ **100 gpm**
- **Wellbore diameter** ➤ **26 in.**
- **Tubing properties** ➤ **Secondary effect**
- **Working fluid properties** ➤ **water**
- **Heat flux/ wellbore depth** ➤ **0.1 W/m² → 5593 m**
- **Formation types** ➤ **Shale (K = 1.89 W/m°C, $\rho c_p = 1875.7 \text{ kJ/m}^3\text{°C}$)**

Best Case Results



- Pseudo steady state fluid return temperature = 98 °C
- Pseudo steady state ideal work rate = 195 kW

Summary and Conclusions

- **Comprehensive sensitivity study conducted**
- **Best Case below existing plant performance**
- **Wellbore heat exchanger not viable even with ideal energy conversion**

Engineered Geothermal Systems using Advanced Well Technologies

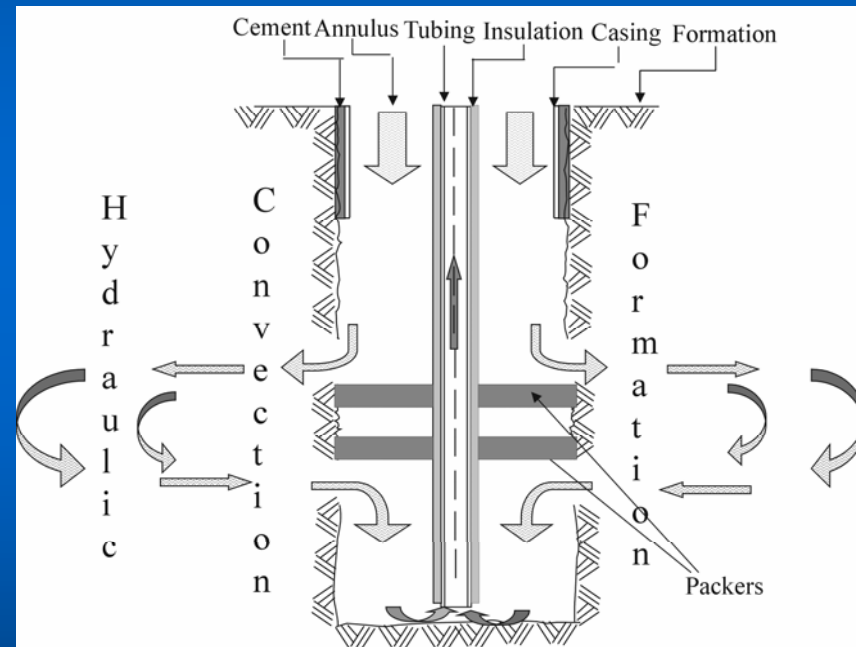
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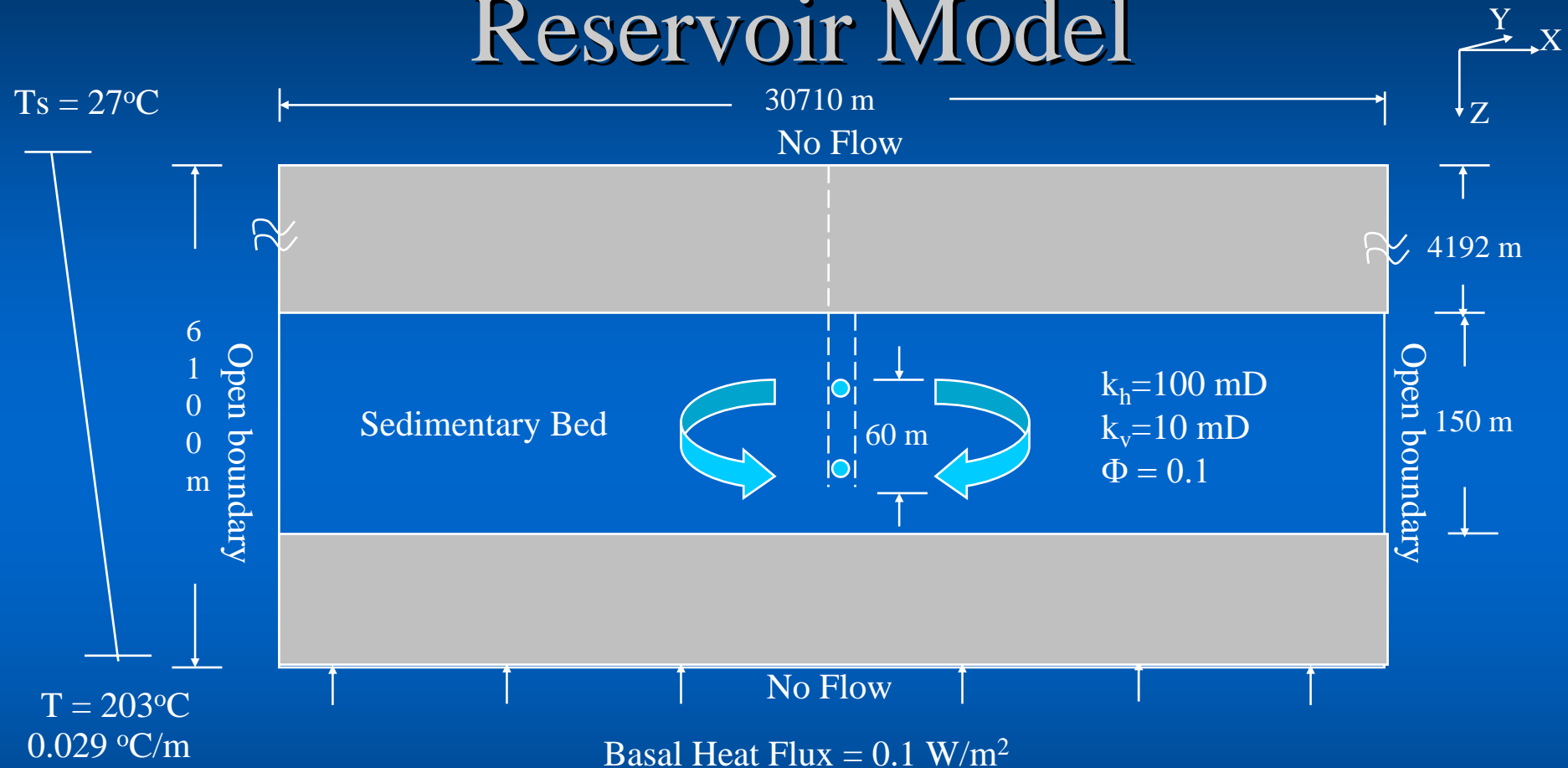
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Vertical Well Dual Perforation (DP) System

- **Geometry**
 - Single vertical well
 - Two perforation intervals with isolation in annulus
 - Vertical hydraulic convection cell
- **Previous Study (Herrling et al., 1990)**
 - Sphere of influence dependent on anisotropy (k_H/k_V) and ratio of screen section lengths over aquifer thickness (a/H)



Reservoir Model



- **Circulation rate = 6.31 kg/s**
- **Injection Temperature = 27°C**

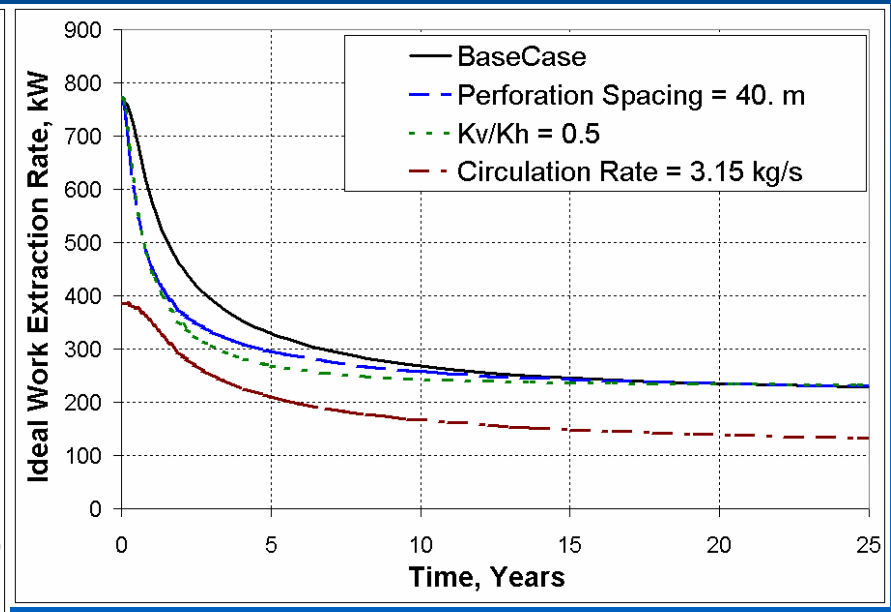
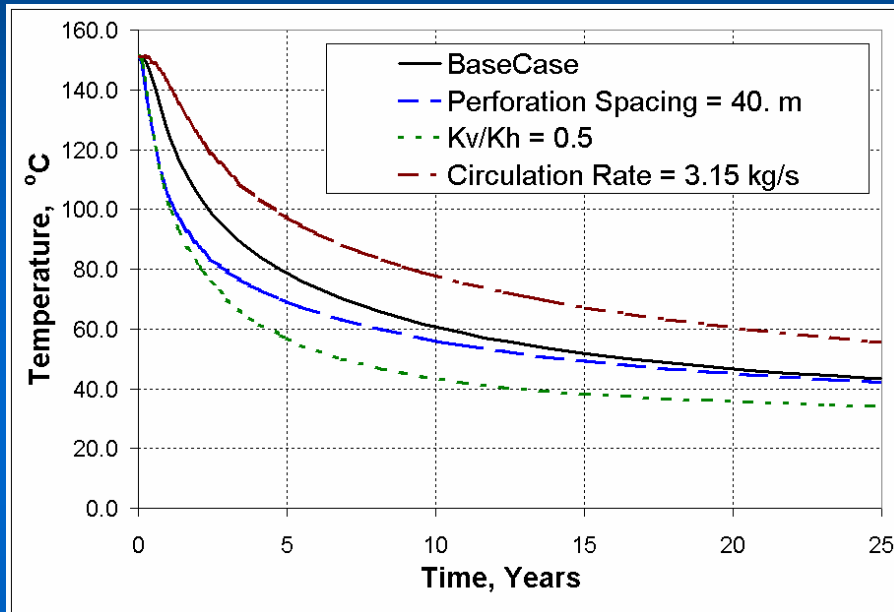
Sensitivity Study

- **Parameters**

- **Vertical/Horizontal Permeability**
- **Circulation Rate**
- **Injection/Extraction Perforation Interval Spacing**

Case Identifier	Perforation Interval Spacing, m	Permeability ratio, k_v/k_H	Circulation Rate, kg/s
Basecase	60.	0.1	6.31
k_v/k_H	60.	0.5	6.31
Circulation Rate	60.	0.1	3.15
Perforation Spacing	40.	0.1	6.31

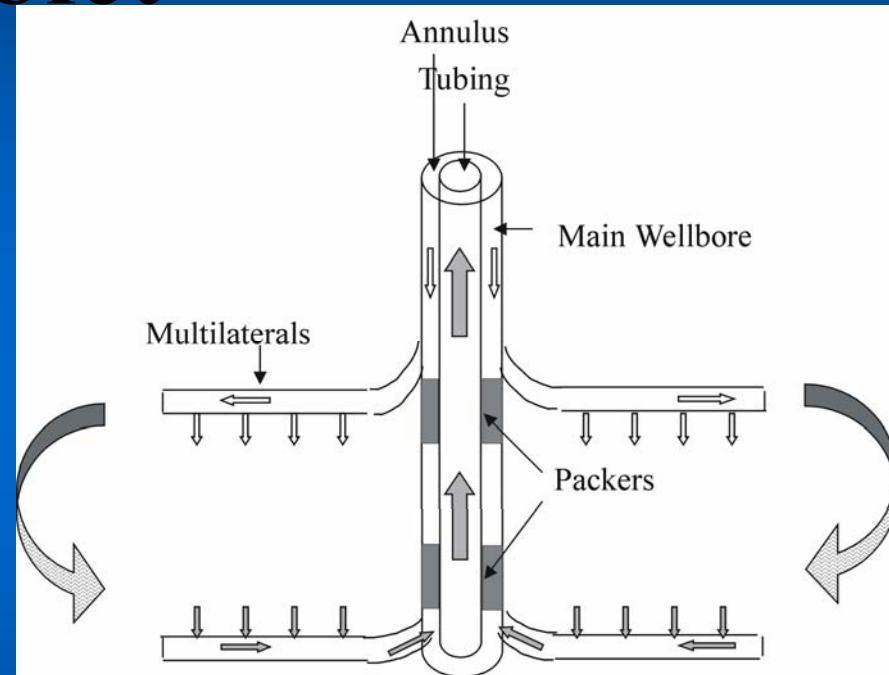
Sensitivity Study



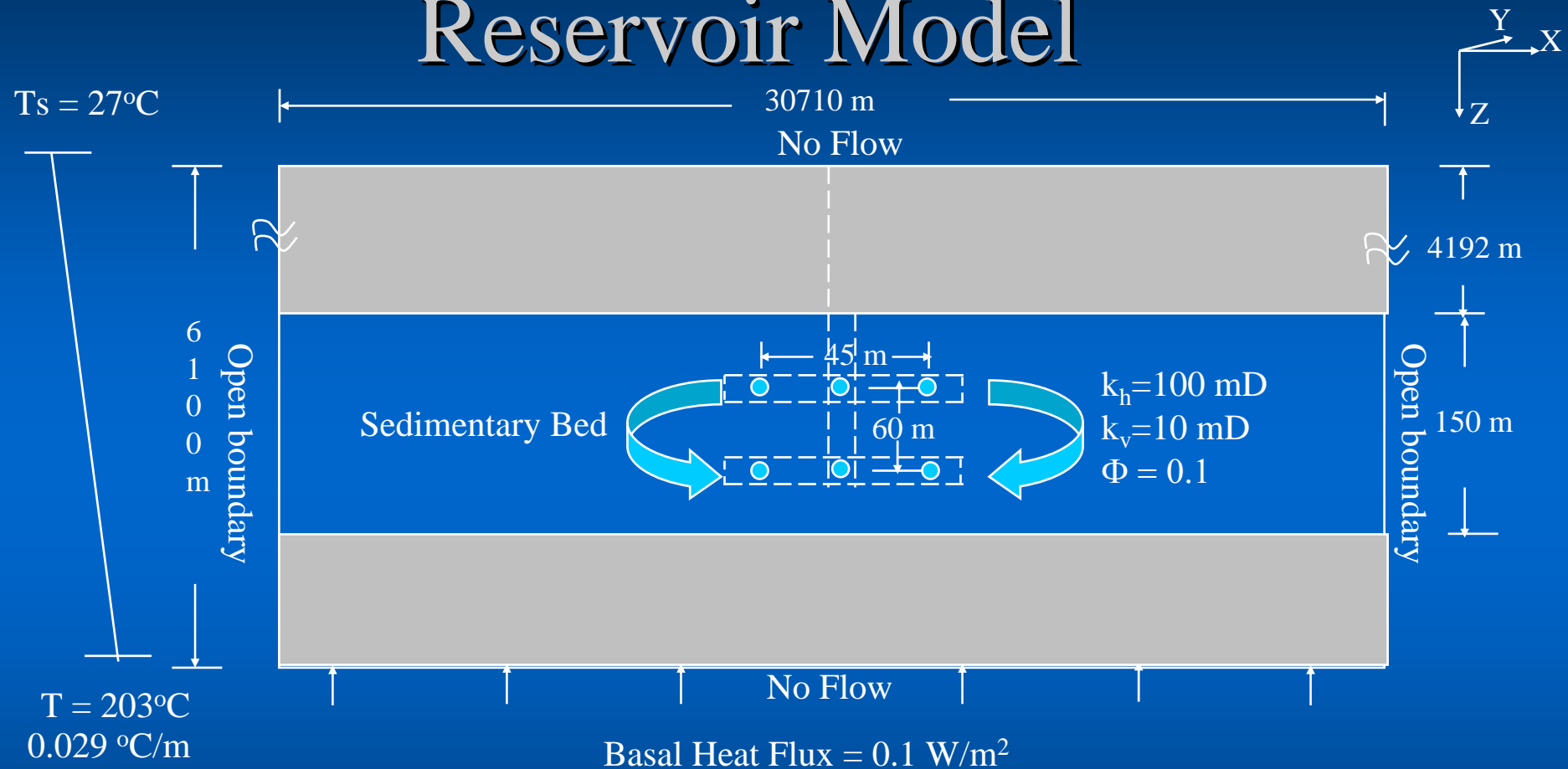
- Reduced vertical spacing → short circuit
- Increased k_v → crossflow & early BT
- Reduced circulation rate → high temperature but low ideal work rate

Vertical Well Dual Lateral Doublet

- **Geometry**
 - Vertical well
 - Dual lateral doublet
- **Improved wellbore productivity and increased reservoir exposure**



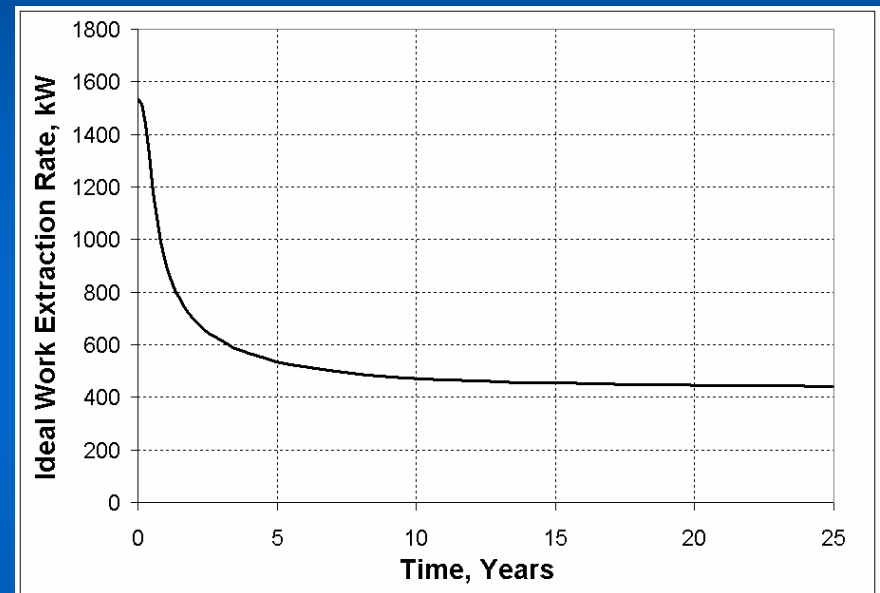
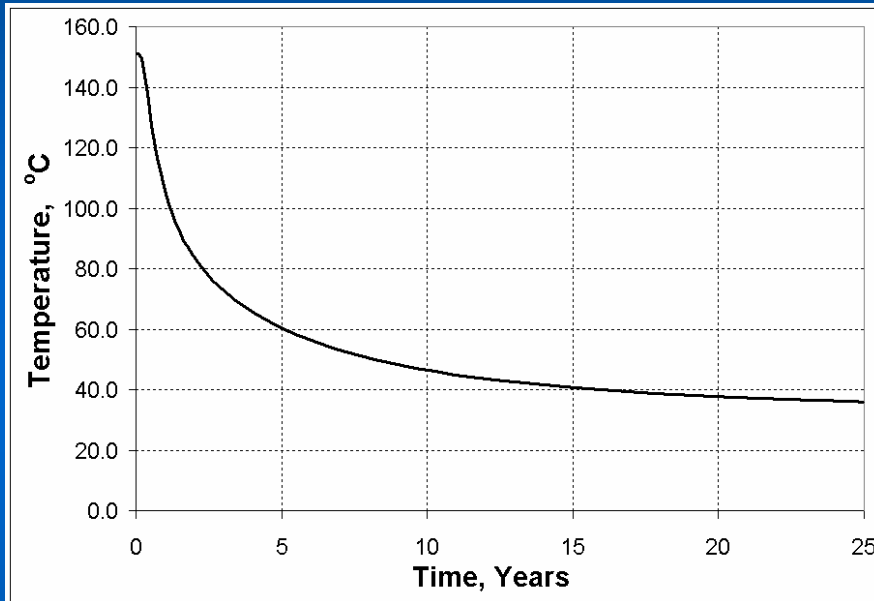
Reservoir Model



Basal Heat Flux = $0.1 \text{ W}/\text{m}^2$

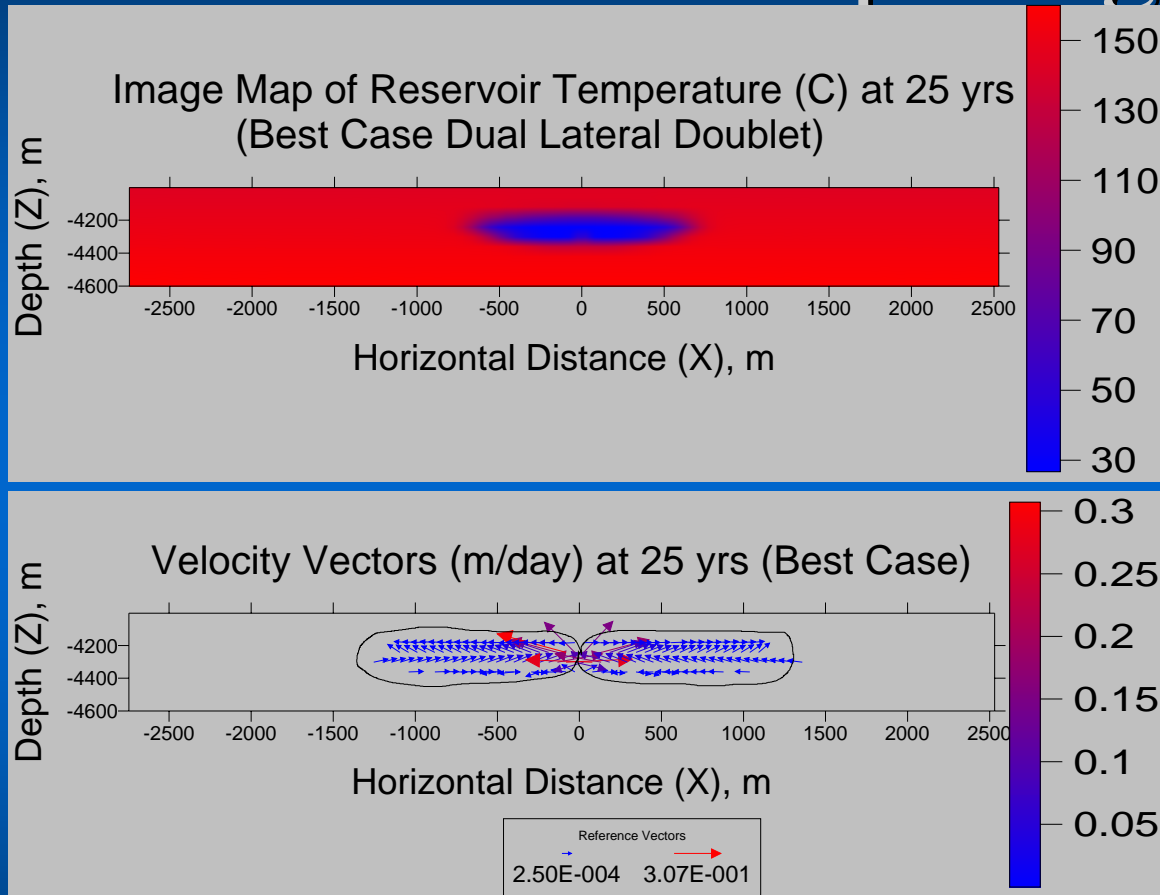
- **Circulation rate = 6.31 kg/s**
- **Injection Temperature = 27°C**

Best Case Dual Lateral Doublet Results

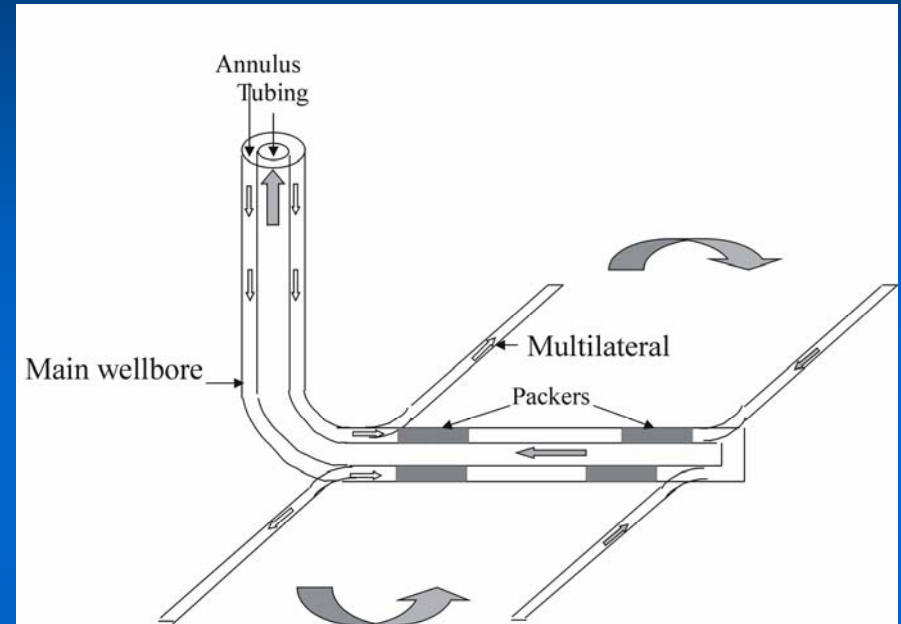
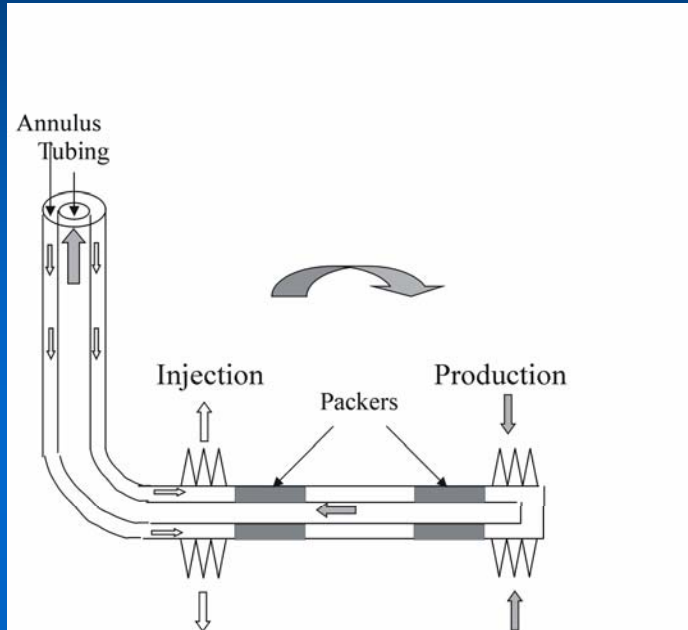


- Best case – Extraction Temperature : 60.4°C & Ideal Work Rate : 536 kW at 5 yrs
- Doesn't incorporate the temperature gain by conduction while flowing down
- Better technology than Dual Perforation for EGS

Thermal/Fluid Swept Region



Future Study



- Horizontal well dual perforation
- Horizontal well dual lateral doublet
- Unconstrained spacing in horizontal wells, higher rock-fluid contact area and higher fluid residence times.

Summary & Conclusions

- **Advanced Well Technologies Evaluation**
 - Preliminary study conducted
 - Potential means of achieving EGS goals
- **Vertical Well Dual Perforation System**
 - Limited by sedimentary bed thickness
- **Vertical Well Dual Lateral Doublet System**
 - Better than Dual Perforation System but still limited sedimentary bed thickness
- **Horizontal Wells**
 - Unconstrained spacing → longer residence times, more rock-fluid contact area and higher temperatures
 - Horizontal well multilateral doublet is promising technology for EGS

Single Well Energy Production

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Governing Equations

- **Single Phase, PSS, inflow equations**
- **Pump efficiency and parasitic load**

$$P_I - P_{wf} = \frac{q\mu}{2\pi kh} \left[\frac{1}{2} \ln \left(\frac{4A}{\gamma C_A r_w^2} + \frac{2\pi kt}{\phi\mu cA} + S \right) \right]$$

Example of Analysis Results

- **Depth = 6 km**
 - $T = 175^{\circ}\text{C}$
- **Reservoir properties**
 - $r_e = 4000 \text{ m}$ ($V_p = 250 \text{ E6 m}^3$)
 - $k > 50 \text{ md}$
 - $h = 25 \text{ m}$
- **$\Delta P = 540 \text{ Bar}$**
 - $P_I = 1005 \text{ bar}$
 - $\cong P_{HS}$ at 12 km
- **No Fluid Replacement option only feasible for geopressured formations**

Injection/Extraction Energy Production

- **Primary production**
 - Offshore production platforms
- **Watered out (mature) fields**
- **Ongoing waterfloods**

Summary

- **EGS attractive in sedimentary basins**
 - Heat transfer A
 - Existing infrastructure
- **No Fluid Replacement restricted to GP**
 - $P_I \gg P_{HS}$
- **Conventional methods using existing petroleum technology good**
 - Waterfloods, production platforms, etc.