Analysis of Groundwater Depletion/Inflation and Freeze–Thaw Cycles in the Northern Urumqi Region with the SBAS Technique and an Adjusted Network of Interferograms

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Abstract: This work investigated the large-scale ground deformations threatening the Northern Urumqi district, China, which are connected to groundwater exploitation and the seasonal freeze–thaw cycles that characterize this frozen region. Ground deformations can be well captured by satellite data using a multi-temporal interferometric synthetic aperture radar (Mt-InSAR) approach. The accuracy of the achievable ground deformation products (e.g., mean displacement time series and related ground displacement time series) critically depends on the number and quality of the selected interferograms. This paper presents a straightforward interferogram selection algorithm that can be applied to identify an optimal network of small baseline (SB) interferograms. The selected SB interferograms are then used to produce ground deformation products using the well-known small baseline subset (SBAS) Mt-InSAR algorithm. The developed interferogram selection algorithm (ISA) permits the selection of the group of SB data pairs that minimize the relative error of the mean ground deformation velocity. Experiments were carried out using a group of 102 Sentinel-1B SAR data collected from 12 April 2017 to 29 October 2020. This research study shows that the investigated farmland region is characterized by a maximum ground deformation rate of about 120 mm/year. Periodic groundwater overexploitation, coupled with irrigation and freeze–thaw phases, is also responsible for seasonal (one-year) ground displacement signals, with oscillation amplitudes up to 120 mm in the zones of maximum displacement.

Keywords: InSAR; small baseline; seasonal ground deformation; linear deformation; irrigated farmlands; reservoir safety; groundwater exploitation; freeze–thaw

1. Introduction

The study of the Earth’s surface displacements through differential SAR interferometry represents a consolidated practice [1–4] at present. In this framework, the last few decades have seen the flourishing of several multi-temporal InSAR (Mt-InSAR) algorithms for the generation of ground displacement time series [5–20]. They can be broadly grouped into two main categories: persistent scatterer (PS) and small baseline (SB) methodologies. The former contains algorithms and tools based on the analysis of pointwise, highly reflective objects (e.g., human-made infrastructures in urban areas) that preserve
high coherence and phase stability even in large temporal and perpendicular baseline SAR data pairs. The techniques in the latter category are primarily devoted to analyzing ground displacement related to distributed scatterers (DSs) on the terrain. DS targets are distributed over multiple resolution cells and are characterized by varying coherence and phase stability. Accordingly, DSs are more prone to phase decorrelation effects [10], especially when the interferometric SAR data pairs have long spatial and temporal baselines. The correct identification of DSs is required, and several techniques are currently available in the literature [19,20]. More recently, new methods for the identification and processing of statistically homogenous pixels (SHPs), based on the use of maximum likelihood (ML) estimators, have also been developed [13–17]. Moreover, some scholars have also presented hybrid Mt-InSAR techniques that jointly analyze PS and DS target ground deformations (e.g., [18]).

Mt-InSAR techniques [21–23] have successfully been applied to monitor the Earth’s ground deformations due to several causes (e.g., earthquakes, volcanoes, landslides and land subsidence). In this context, permafrost regions have also been the subject of several investigations. In particular, ground displacements of permafrost areas have been extensively studied in the North Slope of Alaska [24] and Herschel Island, Canada [25]. Large-scale permafrost freeze–thaw ground deformations were also mapped on the Tibetan Plateau using InSAR data [26–29]. Furthermore, Mt-InSAR methods were applied to map seasonal ground deformations in the high arctic permafrost environment [30], wildfire-induced permafrost ground deformation in the Alaskan boreal forest [31], in Heihe, China [32], and to monitor low-land permafrost areas in the Arctic and Antarctic regions [33]. InSAR observations were used to determine the active layer thickness [34,35] and reveal active layer freeze–thaw and water storage dynamics in permafrost environments [36].

In this work, we investigate the ground deformation of the Northern Urumqi region, China. The presented analysis is based on applying the small baseline subset (SBAS) method [9]. Furthermore, we present a new method for selecting a suitable set of small baseline (SB) interferometric SAR data pairs to be used by the SBAS algorithm. Usually, the interferometric SAR data pairs are selected by merely imposing a threshold on their maximum allowed temporal and perpendicular baselines [9]. However, this selection strategy can lead to some high-quality interferograms being discarded or some low-quality ones being included in actual cases. Some approaches for selecting optimal sets of SB interferograms have already been proposed in the literature [37–43]. In particular, the minimum spanning tree (MST) algorithm was used to determine a set of optimized interferograms using a quasi-PS (QPS) method in [37,38]. The use of a simulated annealing algorithm was proposed in [39] for the optimal selection of a triangular network of SB interferograms that were exploited by the space–time minimum cost flow (EMCF) phase unwrapping algorithm [40]. Graph theory (GT) and a variance–covariance matrix of observations were used in [41] to identify sets of interferograms less influenced by turbulent atmosphere phase artifacts. The semiautomatic selection of optimum image pairs was also proposed in [42], using the coherence of point targets based on a small feature region. A higher coherence pixel density of interferograms through eigenvalue decomposition was introduced in [43].

The SB interferometric selection algorithm proposed in this work was aimed at selecting SB interferograms that would minimize the mean ground deformation velocity relative error. Toward that aim, the average spatial coherence of the chosen interferograms and the connectivity of their network were taken into account at the same time. Our work benefits from the primary outcomes of a recent investigation [44] that addressed the error budget analysis of SB Mt-InSAR techniques.

Experiments were carried out on 102 pieces of Sentinel-1B SAR data collected from 12 April 2017 to 29 October 2020. Starting from the available SAR data, a group of optimal SB interferograms was adequately selected and used within the SBAS processing. As a result, in the region of maximum deformation, we revealed a ground subsidence velocity of about 120 mm/year and seasonal amplitude displacement of about 120 mm.
This paper is organized as follows: Section 2 describes the methods used in this research study. Section 3 illustrates the study area. Experimental results are shown in Section 4. Finally, discussions and conclusions are given in Section 5 and Section 6, respectively.

2. Methodology

This section summarizes the rationale of the SBAS methodology [9] and describes the novel interferometric SAR data pair selection algorithm.

2.1. Rationale of the SBAS Method

Let us consider a group of \( N \) SAR images acquired at chronologically ordered times \( [t_0, t_1, ..., t_{N-1}]^T \), from which a set of \( M \) small baseline (SB) interferometric SAR data pairs is selected. Once selected, a group of optimized \( M \) SB multi-look interferograms is generated and unwrapped. Let \( \Delta \psi^{(SB)} = [\Delta \psi_0^{SB}, \Delta \psi_1^{SB}, ..., \Delta \psi_{M-1}^{SB}]^T \) be the vector of the unwrapped phases related to a generic coherent SAR pixel. The ground displacement time series are obtained by solving the following system of linear equations [9]:

\[
B \cdot \upsilon = \Delta \psi^{(SB)} \tag{1}
\]

where \( B \) is the design matrix of the involved linear transformation (see [9] for the mathematical expression of matrix \( B \)), and \( \upsilon \) is the vector \( \upsilon = \left[ \frac{\phi_i - \phi_i}{t_i - t_i}, \frac{\phi_i - \phi_i}{t_i - t_i}, ..., \frac{\phi_i - \phi_i}{t_i - t_i} \right]^T \), whose (unknown) elements represent the ground velocity estimates between consecutive time acquisitions. Note that \( \Phi = [\phi_0, \phi_1, ..., \phi_{N-1}]^T \) is the vector of the (unknown) phases (i.e., the phase time series) related to every available SAR acquisition. Once estimated, the elements of vector \( \upsilon \) are time-integrated, and phase \( \Phi \) is retrieved. The residual topographic errors and the atmospheric phase screen (APS) are finally estimated and compensated to obtain the ground displacement time series [9]. After the SBAS inversion, the quality of the reconstructed ground deformation time series can be checked by calculating the value of the temporal coherence factor [40]. The temporal coherence depends on the phase residuals \( R = B \cdot \hat{\upsilon} - \Delta \psi^{(SB)} \) of the LS problem of Equation (1) and is defined as follows:

\[
\Omega = \frac{1}{M} \sum_{i=0}^{M-1} \exp \left[ jR_i \right] \tag{2}
\]

Finally, a group of well-processed, highly coherent SAR np pixels, characterized by values of temporal coherence larger than a given threshold, is identified.

2.2. SBAS Deformation Measurement Accuracy

A recent work [44] comprehensively addressed, from the theoretical perspective, the problem of deriving some bounds for the relative errors of Mt-InSAR SB products. In particular, using the basic principles of perturbation and error propagation theory [45–47], it has been shown that the expected relative error \( \epsilon_{\upsilon} \) of the computed vector \( \hat{\upsilon} \) (i.e., the solution of the least-squares problem of Equation (1)) is given by:

\[
\epsilon_{\upsilon} = \frac{\| \hat{\upsilon} - \upsilon \|}{\| \upsilon \|} \leq \varepsilon \left( \frac{2k(B)}{\cos \eta} + \tan \eta \cdot k^2(B) \right) + O(\varepsilon^2) \tag{3}
\]

where \( \upsilon \) is the vector of the actual (unknown) velocities among consecutive time acquisitions; \( k(B) \) is the condition number of the matrix design \( B \), which can be calculated as \( k(B) = \sigma_0 / \sigma_{\text{min}} \), where \( \sigma_0 \) and \( \sigma_{\text{min}} \) are the largest and smallest non-zero singular values.
of matrix $B$. Additionally, $\varepsilon = \frac{\| \Delta \Psi^{(SB)} - \Delta \tilde{\Psi}^{(SB)} \|_2}{\| \Delta \tilde{\Psi}^{(SB)} \|_2}$ is the relative error of the SB unwrapped phases, where $\Delta \Psi^{(SB)} = 4\pi d/\lambda$, $d = [d_0, d_1, \ldots, d_{M-1}]^T$ is the vector of ground deformations related to the $M$ selected interferometric SAR data pairs, and $\lambda$ is the operational wavelength. Moreover, $\eta = \arcsin \left\{ \frac{\| R \|}{\| \Delta \Psi^{(SB)} \|} \right\}$, where $R = B \cdot \tilde{\Psi} - \Delta \Psi^{(SB)}$ is the vector of the least-squares (LS) residuals. Note that $\| X \|_2$ is the two-norm of the generic $(Q \times 1)$ vector $X = [x_0, x_1, \ldots, x_{Q-1}]^T$, which is given by $\| X \|_2 = \left[ E \left( X^T \cdot X \right) \right]^{1/2}$.

2.3. Optimal SB Data Pair Selection

This subsection presents a straightforward algorithm for the automatic selection of a reliable group of SB SAR data pairs to be used within the SBAS algorithm. The algorithm does not simply impose some fixed thresholds on the temporal and perpendicular baselines of the data pairs. Instead, it directly analyzes the average coherence of the generated interferograms and considers the characteristics of the selected network of SB interferograms to identify the network that allows minimizing the (expected) relative error of the ground deformation velocity. In particular, for the SBAS case, Equation (3) shows that the relative error of vector $V$ depends on the noise corrupting the set of SB unwrapped interferograms, which is determined by the relative error of the exploited unwrapped interferograms and the condition number of the matrix design $B$. For the sake of simplicity, the adopted strategy assumes the idealized case in which no significant phase unwrapping errors (and other spurious time inconsistencies) are present. Accordingly, the norm of the LS residuals is minimal. Under this hypothesis, we can suitably assume that $\eta \geq 0$, and the error bound of Equation (3) is particularized as:

$$\varepsilon_{\text{c}} \leq 2\varepsilon k(B)$$

(4)

Under the validity of the Cramér–Rao bound for the variance of the SB interferograms [48], the relative error of the unwrapped (multi-look) interferograms can be approximated with:

$$\varepsilon = \frac{\| \Delta \Psi^{(SB)} - \Delta \tilde{\Psi}^{(SB)} \|_2}{\| \Delta \tilde{\Psi}^{(SB)} \|_2} \approx \frac{\lambda}{4\pi d \|_2} \sqrt{\frac{1}{2M} \sum_{i=0}^{M-1} \left( 1 - \frac{1}{\pi^2_i} \right)}$$

(5)

where $\Gamma = [\pi_0, \pi_1, \ldots, \pi_{M-1}]^T$ is the vector of the (average) coherence value of the used $M$ SB SAR data pairs, and $L$ is the look number. By substituting Equation (5) into Equation (4), we get:

$$\varepsilon_{\text{c}} \leq \frac{\lambda}{2\pi d \|_2} \sqrt{\frac{1}{2L} \sum_{i=0}^{M-1} \left( 1 - \frac{1}{\pi_i^2} \right)} k(B) = \alpha \cdot \beta \cdot k(B)$$

(6)

where the term $\alpha = \frac{\lambda}{2\pi d \|_2} \sqrt{\frac{1}{2L}}$ depends on the system parameters and the ground deformation norm, whereas the term $\beta = \left[ \sum_{i=0}^{M-1} \left( 1 - \frac{1}{\pi_i^2} \right) \right]$ accounts for the average coherence of the SB interferograms. Note that the norm of the (true) ground deformation does not depend (at most) on the selected SB interferograms but is a specific parameter of the
investigated area. Thus, the developed interferogram selection algorithm (ISA) focuses on minimizing the term $\beta \cdot k(B)$.

The ISA method consists of 3 distinctive steps to determine the optimal set of SB interferograms, which is briefly summarized as follows:

I. Generate a pool of (candidate) multi-look SB interferograms and the relevant coherence maps. Candidate SB data pairs are initially selected by considering a reasonably large threshold for the temporal and perpendicular baselines of the interferograms.

II. Estimate the optimal value of a coherence threshold, namely $\gamma_{\text{critical}}$, which is the coherence threshold that allows minimizing the term $\beta \cdot k(B)$ given the selected set of SB interferograms. When a given multi-look SAR interferogram has an average spatial coherence smaller than $\gamma_{\text{critical}}$, it is discarded from the subsequent analyses.

III. Apply the SBAS procedure [9] to the selected set of optimal SB SAR data pairs, selected using the optimal coherence threshold $\gamma_{\text{critical}}$.

A block diagram of the developed ISA is shown in Figure 1.

Figure 1. Flowchart of developed SB interferogram selection algorithm.

3. Case Study Area

Northern Urumqi, China, is located between the Tianshan Mountains and the Gurbantunggut Desert (Figure 2). The average altitude is about 500 m. The area belongs to the middle temperate continental arid region, characterized by long winter and summer seasons [49]. In particular, during winter, from the middle of October to the middle of the following March, the temperature is usually constantly below $0^\circ$C. More than 50 rivers originate in the north of the Tianshan Mountains, supplied by snow cover and melting glaciers. The annual average runoff can reach $82.7947 \times 10^8$ m$^3$ [50]. Dense rivers form a large arid alluvial plain in the north of the Tianshan Mountains and gradually develop into typical irrigation agriculture under human activity.
Irrigated agriculture is relatively developed here, one of China’s essential grain production bases. Moreover, since the implementation of the national policy to develop Xinjiang, agricultural land reached 22,330 km² by 2010, accounting for about 17% of the region’s total land area [51]. The main crops include wheat, corn, melons, fruits and cotton. Agricultural irrigation mainly depends on groundwater and river water. The farmland area is primarily irrigated using river water, whereas areas far from rivers and reservoirs can only rely on groundwater. Many reservoirs are located in the study area, as shown in Figure 2. They store surface water during the rainy season and snowmelt during the spring season. Stored groundwater is then pumped during the summer season to facilitate agricultural irrigation. However, due to the limited surface runoff, groundwater demand has exceeded recharge capacity in agricultural production. In addition, in the permafrost areas, freeze–thaw deformation phenomena occurred.

The average annual temperature of the study area is 6.7–8.9 °C; the average yearly precipitation is 224.28 mm, and the average annual sunshine amounts to 2671.5 h. These conditions create distinctive agricultural resources. There is an excellent climate for agricultural development [52]. However, water consumption for agricultural irrigation is substantial, especially in dry areas. From 1988 to 2015, water consumption for irrigation increased by 256%, and the water consumption of crops increased year by year [53]. The proportion of agricultural water consumption was 92.5% in 2017. Overexploitation of groundwater leads to decreased pore water pressure and land subsidence on irrigated farmland.
4. Experimental Results

4.1. SBAS Ground Deformation Time Series Generation

This research study exploited 102 pieces of Sentinel-1B SAR data collected from 12 April 2017 to 29 October 2020. Table 1 summarizes the main data parameters.

<table>
<thead>
<tr>
<th>Sensor</th>
<th>Sentinel-1B</th>
</tr>
</thead>
<tbody>
<tr>
<td>Time span</td>
<td>12 April 2017 to 29 October 2020</td>
</tr>
<tr>
<td>Number of SAR images</td>
<td>102</td>
</tr>
<tr>
<td>Incidence angle</td>
<td>39.14°</td>
</tr>
<tr>
<td>Beam mode</td>
<td>IW</td>
</tr>
<tr>
<td>Flight direction</td>
<td>Descending</td>
</tr>
<tr>
<td>Path</td>
<td>19</td>
</tr>
<tr>
<td>Frame</td>
<td>444</td>
</tr>
<tr>
<td>Pixel spacing (range × azimuth)</td>
<td>2.3 m × 14.9 m</td>
</tr>
</tbody>
</table>

We applied the developed ISA method to the available SAR images to identify an optimized group of SB multi-look interferograms that the conventional SBAS technique has subsequently processed. To this aim, we preliminarily identified a group of “candidate” SB SAR data pairs characterized by the maximum temporal baseline $\Delta t_{\text{max}} = 90$ days, and we did not apply any constraint on the maximum perpendicular baseline of the interferograms. Figure 3A shows the distribution of preselected SB interferometric SAR data pairs in the temporal/perpendicular baseline plane. In this domain, the available SAR images are represented by red circles. The arcs connecting pairs of SAR data (drawn in blue) identify the set of candidate SB SAR data pairs. Once identified, a group of 656 SB multi-look interferograms was generated.

Precise satellite orbit information and a three-arcesec digital elevation model (DEM) of the area from the Shuttle Radar Topography Mission (SRTM) were used to estimate and remove the topographic phase components. The generated interferograms were independently multi-looked (10 range–2 azimuth looks, respectively) and noise filtered with the use of the Goldstein filter [2] (with alpha = 0.6). Contextually, we also generated the corresponding coherence map for every generated differential SAR interferogram and computed the relevant average coherence value (over the whole imaged area). Figure 4A shows how the average coherence drops as the temporal baseline of the interferograms increases; however, because the S-1 orbital tube is narrow, there is no substantial decoherence strictly related to the perpendicular baselines.

At this stage, we applied the developed ISA method and identified the optimal set of SB interferograms that minimized the term $\beta \cdot k(B)$ (see Section 2). We note that, as the applied threshold on the minimum (average) spatial coherence $\gamma_{\text{thresh}}$ increases, two opposite effects occur: (i) the multi-look interferograms are less affected by decorrelation artifacts, and (ii) the number of interferograms with average coherence greater than $\gamma_{\text{thresh}}$ drops. These counteracting effects are taken into account by $\beta$ and $k(B)$, respectively. Note that in the limit case, the threshold $\gamma_{\text{thresh}}$ leads to the formation of two independent sets of SB interferograms, and the condition number $k(B)$ becomes infinite as the relative error bound (Equation (6)). In this case, unless there is a substantial time overlap between the two independent subsets of SAR data, the singular value decomposition of matrix B is exploited to solve the least-squares (LS) problem of Equation (1).

Figure 5A,B show the plots of $\beta$ and $k(B)$, respectively, as a function of the average coherence threshold. Figure 5C plots the value of $\epsilon$ versus the average spatial coherence threshold $\gamma_{\text{thresh}}$, highlighting that the optimal condition arises, in our specific case, considering an optimal coherence threshold $\gamma_{\text{critical}} = 0.84$ (P1 in Figure 5C). In this
case, an adjusted/optimal network of 421 SB multi-look interferograms is determined. Figure 3B shows the distribution of the selected optimal SB interferometric SAR data pairs in the temporal/perpendicular baseline domain. In Figure 5C, P2 highlights the limit case when only one single interferogram exists to connect two subsets of SB interferograms (e.g., the condition number is maximum but not infinite). This condition corresponds to $\gamma_{\text{thresh}} = 0.86$ and to a group of 389 SB differential SAR interferograms in our experiment. Figure 4C shows the distribution of SB interferometric SAR data pairs in the temporal/perpendicular baseline domain for this limit case.

Figure 3. Distribution of SAR data pairs in a temporal/perpendicular baseline domain. (A) Set of available SB InSAR data pairs estimated by imposing a maximum temporal baseline separation of 90 days. (B) Optimal network of SB interferograms retrieved by applying the proposed InSAR selection algorithm. (C) Reduced network of SB interferograms at boundary condition where one single SB data pair exists that connects the group of interferograms to form a single set of data. Note that (B) and (C) refer to the condition on minimum average spatial coherence of selected interferograms of 0.84 (P1 in Figure 5C) and 0.86 (P2 in Figure 5C).
Figure 4. Scatter plot of average spatial coherence of candidate SB data pairs vs. their (A) temporal and (B) perpendicular baseline.

Figure 5. Plots of (A) $\beta$, (B) $k\beta$, and (C) $\beta \cdot k\beta$ vs. the interferometric average spatial coherence threshold.

Some coherence maps are shown in Figure 6. Mainly, Figure 6A,B shows the coherence map of the worst interferogram (i.e., characterized by the minimum average spatial coherence) for the optimal case (P1 in Figure 5C) and the limit case (P2 in Figure 5C), respectively. Furthermore, Figure 6C shows the coherence map of the best interferogram for the whole selected optimal SB interferogram network, and Figure 6D shows the coherence map of the worst candidate, the SB interferogram. The latter does not belong to the set of interferograms used for the SBAS inversion. The master and slave SAR images of the selected SAR data pairs are listed in the caption of Figure 6.

Figure 6. Spatial coherence maps of four DInSAR SB interferograms. The worst coherence images related to selected optimal set of SB interferograms (P1 condition, Figure 5C) and limit case (P2 condition, Figure 5C), respectively: (A) the coherence map of 18 February 2018 to 26 March 2019 InSAR data pair (average coherence 0.84) and (B) the coherence map of 2 November 2017 to 25 January 2018 (average coherence 0.86). (C) The best coherence map as a whole related to the 20 January 2019 to 1 February 2019 InSAR data pair (average spatial coherence 0.99). (D) The worst coherence map as a whole in the set of candidate SB InSAR data pairs related to the 13 February 2019 to 8 May 2019 InSAR data pair (average spatial coherence 0.28). Although (D) is related to an SB InSAR data pair, it must be discarded to enhance the quality of ground deformation products.
Starting from the optimized set of 421 SB interferometric SAR data pairs shown in Figure 3B, we applied to the relevant multi-look differential interferograms the conventional SBAS-InSAR processing in the implementation provided in the StaMPs software package [18] to generate the ground deformation time series related to stable DS targets. The DS target locations were identified by the phase stability analysis [18] provided in the StaMPs software package. StaMPs implementation processing can be found in [54]. Accordingly, a group of about 3.7 million pixels was selected. Over these pixels, the phase unwrapping operations [55] were implemented to reconstruct the relevant (full) unwrapped phases.

Multi-look unwrapped phases were inverted, pixel by pixel, using the SBAS approach, and the ground deformation time series relevant to the set of coherent SAR pixels were computed. To check the quality of the generated ground displacement time series, we calculated the values of the temporal coherence factor [40], which indirectly measures the probability error of the ground deformation measurements. Temporal coherence has been widely used in SBAS investigations [56–58] over the years, and a threshold value of 0.7 is considered legitimate for reliable DInSAR ground deformation products. Large temporal coherence values mean the ground deformation time series are consistent with the measured interferometric phases.

Figure 7 shows the map of temporal coherence. Note that areas with a low temporal coherence value (less than 0.7) are mainly concentrated on the mountains (the lower right corner). Accordingly, these areas were excluded from subsequent analyses. Figure 8A shows the map of ground mean deformation velocity of the investigated area over well-processed radar pixels. Six points, labeled A–E in Figure 8A, were identified in the studied region, whose relevant ground displacement time series are shown in Figure 9. They show that ground deformation time series over the investigated area contain a linear component in time (subsidence), superimposed with a nonlinear seasonal component over an approximately one-year period.

Figure 7. Map of temporal coherence.
To further check the reliability of the obtained SBAS-driven ground deformation results and to prove the effectiveness of the developed ISA, we also generated, using the SBAS technique, the ground deformation time series of the area using the networks of SB interferograms shown in Figure 3A,C, consisting of 656 and 389 SB multi-look interferograms, respectively, the use of which corresponds to the use of “candidate” SB interferograms (A) and the set of interferograms at the limit case. The three generated families of ground displacement time series were jointly analyzed to infer their accuracy. Unfortunately, there is a lack of external, freely available GPS/leveling measurements for validation purposes.
Figure 9. Deformation, temperature and rainfall time series comparison at six points, A–F (as described in Figure 8). The first line is a rainfall and temperature time series. (A–F) deformation including observation, linear and seasonal deformation time series, respectively. Vertical dotted black and green lines show the inflection points of seasonal term deformation.

To partially circumvent this problem, we adopted the following strategy. For every family of ground displacement time series, we extracted the relevant spatial low-pass (LP) and high-pass (HP) ground deformation time series (using a moving average window of 10 × 10 pixels). Assuming that the (true) ground deformation is spatially correlated in the averaging box, and considering that the APS is also spatially correlated, we can reasonably assume that the HP components are mainly sensitive to the decorrelation noise and phase unwrapping errors. Thus, an indirect measure of the accuracy of the ground displacement time series could be given by the standard deviation of the HP components in an area of interest. Figure 10 shows a histogram of the HP standard deviation for the three networks of SB interferograms used in this study, as computed over a box centered around the location of point C (see Figure 8B). The values of the average HP standard deviation are 1.56, 1.29 and 1.38 mm for the three SB networks. The result of this experiment shows that the selected optimal SB interferogram network leads to the generation of ground displacement time series that are less noisy.
4.2. Analysis of Ground Deformation Signals

Let us now focus exclusively on the ground deformation time series related to the optimal SB network of interferograms, shown in Figures 8 and 9. In analyzing these time series, first we discriminated the linear and nonlinear ground deformation components in time. Pixel by pixel, we estimated the linear components by simply fitting the ground displacements with a line. We then subtracted the linear components from the ground deformation time series. We provided the residues, in the LS sense, with a sinusoidal model, \( A\sin(2\pi t/T) \), using a least-squares sine fitting algorithm (e.g., [59]), where \( A \) and \( T \) are the amplitude and period of oscillations. It is worth noting that more sophisticated approaches, such as independent component analysis (ICA) [60–63], could also be applied to infer the periodical ground deformation components. Figure 8B shows, for every well-processed SAR pixel, the map of amplitudes of periodical (over a period of approximately one year) sinusoidal ground displacements. Of course, this model well fits the ground deformations in the farmland regions, where the deformation signals can be related to groundwater depletion and inflation during a period of one year. Conversely, the quality of fitting deteriorates in other zones of the case study area.

The observed terrain displacement time series were also compared to temperature (blue lines) and rainfall (green histograms). The measured ground displacement time series were decomposed into their main components: long-term linear trend (green lines) and nonlinear seasonal deformation (black lines) time series. The rainfall data and temperature were from [64,65]. The rainfall time series, temperature and deformation time series were mapped to interpret the cause of the deformation pattern. The vertical dotted black and green lines identify the beginning and end of the irrigation periods (approximately from April to October every year), corresponding to the peaks (uplift and subsidence) of seasonal ground displacements.

Let us now focus on the area highlighted by the rectangular black box in Figure 8B. Figure 11 shows a zoomed view of the Bayi Reservoir area. The reservoir was built in 1952 with a catchment area of 15 square kilometers. Its storage capacity reaches 35 million cubic meters for water storage and agricultural irrigation. The west of Bayi Reservoir is a
farmland area, and the loss of groundwater causes large-scale land subsidence and threatens the safety of the reservoir. Around the Bayi Reservoir, the linear deformation rate exceeds 40 mm/year (Figure 11B), and the amplitude of seasonal deformation magnitude reaches 120 mm/year (Figure 11C). The deformation pattern includes linear and seasonal deformation. The observed ground deformations represent a threat to the ecological balance and wastewater resources of the area. Figure 11D shows the ground deformation time series of the selected point P. We find that the magnitude of deformation, including seasonal and linear deformation, is low in the non-farmland area. Conversely, in the farmland area (between Qinggeda Lake and Bayi Reservoir), seasonal deformation is high.

5. Discussion

Figure 11. (A) Zoomed view of the optical image shown in Figure 8, corresponding to Bayi Reservoir and Qinggeda Lake. (B) Mean deformation velocity map. (C) Map of seasonal deformation amplitude values. (D) Plot of the ground deformation time series related to point P, highlighted by a black arrow in (B).
In this section, we discuss our research findings by focusing on the proposed ISA method and the primary outcomes of the SBAS investigation in the considered case study area.

One of the main achievements of our investigation was that we developed and preliminarily checked the potential of a novel strategy to automatically select small baseline interferometric SAR data pairs that the SBAS DInSAR technique can use. The selected SB network is the result of a compromise, considering both the effects of the average coherence of the SB interferograms and the connectivity of the resulting SB network. Too few interferograms might lead to SB networks that are less redundant. Thus, even minor errors in single multi-look interferograms, such as phase unwrapping errors, can severely corrupt the generated ground deformation time series. On the other hand, too many interferograms might lead to noisier ground deformation time series due to the presence of interferograms that are more decorrelated, even using SAR data pairs with small temporal and perpendicular baseline separations. Phase decorrelation also magnifies the phase unwrapping errors that can propagate from noisy interferograms to good interferograms due to the SB network redundancy. Therefore, it is mandatory to find a proper balance between these two distinctive effects. The proposed ISA aims to find such a balance condition. The optimal set of interferograms can be used to investigate surface deformations in large-scale areas rapidly to obtain ground deformation time series.

The results of the experiments shown in Section 4.1 (Figure 10) demonstrate that the accuracy of SBAS ground deformation time series improves when the optimal network of SB interferograms is used. We note that some assumptions were made to obtain these results; specifically, we assumed that ground deformations are spatially correlated. Certainly, further extended analyses are required to quantitatively assess the performance of the developed ISA method.

With the results obtained from the SBAS analyses performed in the selected case study area, we derived ground deformation time series. We inferred the sources of ground deformations, discriminating long-term zone deformations (linear trend) from seasonal deformations related to one-year irrigation and the freeze–thaw cycles of the frozen area under investigation. In terms of water consumption, the study area is located between deserts in the north and the Tianshan Mountain in the south.

The observed land subsidence in the farmland areas is related to irrigation methods and facilities related to groundwater recharge and consumption, as shown in Figure 8B, where the amplitude of seasonal ground displacements is shown. Notably, we noticed that these seasonal changes are superimposed over a general trend of subsidence of irrigated land that has evolved over recent years (2017 to 2020). The small-scale land subsidence caused by overexploitation of groundwater in the Northern Urumqi region has been investigated [66].

The analysis of the plots shown in Figure 11 shows that the deformation time series are moderately correlated to temperature variations. Note that in the study areas, the temperature difference in a year is enormous; the highest temperature is 41 °C and the lowest is −28 °C. In these areas, instead of permafrost, temperature changes can lead to freezing and thawing. Moreover, our results suggest that the observed ground deformation is mainly related to the yearly farmland irrigation cycle, which usually starts in March/April and ends in October. This is in agreement with what is shown by the nonlinear deformation time series of points A-F depicted in Figure 11. Of course, there is a correlation between seasonal temperature variations and irrigation cycles. This is the reason for the inferred moderate correlation between ground displacement and temperature. Our results are in general agreement with the outcomes of a research study [66] that investigated small-scale ground deformations linked to irrigation in the Northern Urumqi region by using first-generation ENVISAT/ASAR images collected from 2003 to 2009.

It is documented that rainfall and temperature have little influence on the groundwater level changes in this area [67]. Accordingly, most of these changes can be related to human activities and particularly to the irrigation of farmland. Indeed, the starting and
stopping of agricultural irrigation strictly regulates groundwater depth [67]. Mainly during the agricultural irrigation period, subsidence deformation is caused by the overexploitation of groundwater. In the period when irrigation activities are stopped, uplift deformation depends on the recharge of groundwater [66]. These seasonal groundwater level changes thus have an impact on the observed nonlinear ground deformation, as shown in Figure 11, where the dotted green and black lines highlight the beginning and end of the irrigation period. As a final remark, from our data analysis, we also underline that in this area, the ground displacements driven by irrigation are more significant than those due to the expansion and contraction of the terrain caused by freezing and thawing, which represent the second-order factor that is superimposed on the observed nonlinear ground deformations.

6. Conclusions

In this paper, we propose a novel strategy for selecting an adjusted network of SB interferograms to be subsequently used by the conventional SBAS technique to obtain ground deformation time series. The developed interferogram selection method aims to minimize the relative error of mean ground displacement velocity measurements based on the primary outcomes of recent theoretical studies. Further efforts are still required to generalize the method to consider other quality parameters of the selected interferograms and take into account the effects of phase unwrapping errors and APS artifacts in order to select the optimal set of SB interferograms. The developed ISA was first tested considering Sentinel-1B SAR data acquired over the farmland area of the Northern Urumqi region, China. Of course, evaluating the capabilities of the developed method would require applying it to several case study areas. However, this is a matter for future investigation. Concerning the results obtained by applying this method to the investigated region, we note that SBAS analysis showed that the primary source of the observed ground deformations is primarily related to the overexploitation of groundwater for farmland irrigation. The groundwater in arid areas is of great significance to maintain the stability of the ecosystem. Thus, in areas where water resources are scarce, to ensure the healthy development of agriculture, it is very important to change the traditional irrigation methods and improve the utilization rate of water resources.

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